

IMPROVED SLAG QUALITIES BY LIQUID SLAG TREATMENT

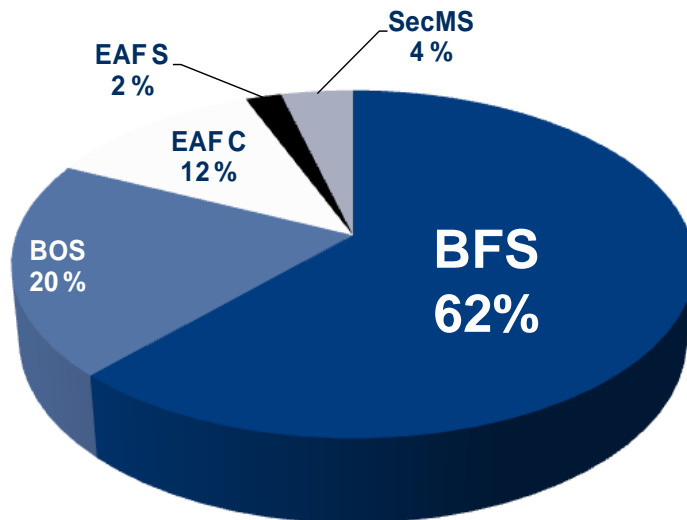
D. MUDERSBACH,
P. DRISSEN, H. MOTZ



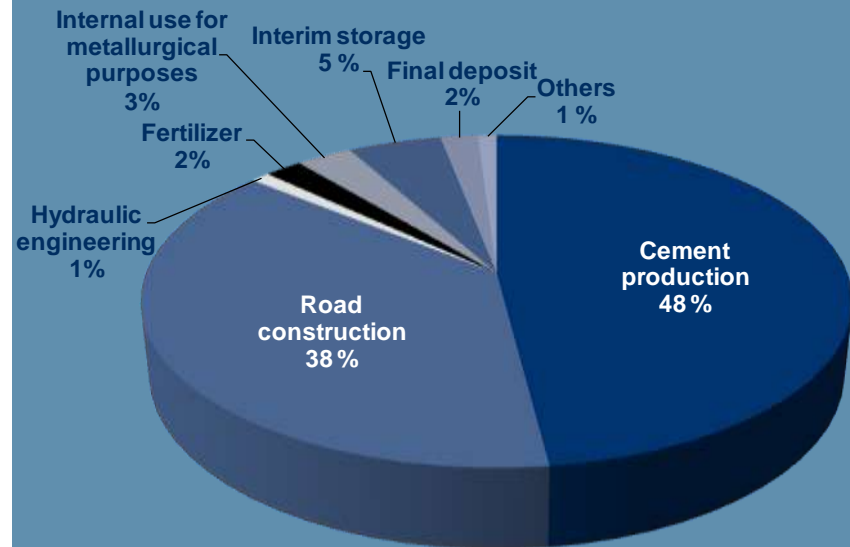
Introduction

IMPROVED SLAG QUALITIES BY LIQUID SLAG TREATMENT

Production of Iron and Steel Slag in Europe 2008: 45.6 million tonnes

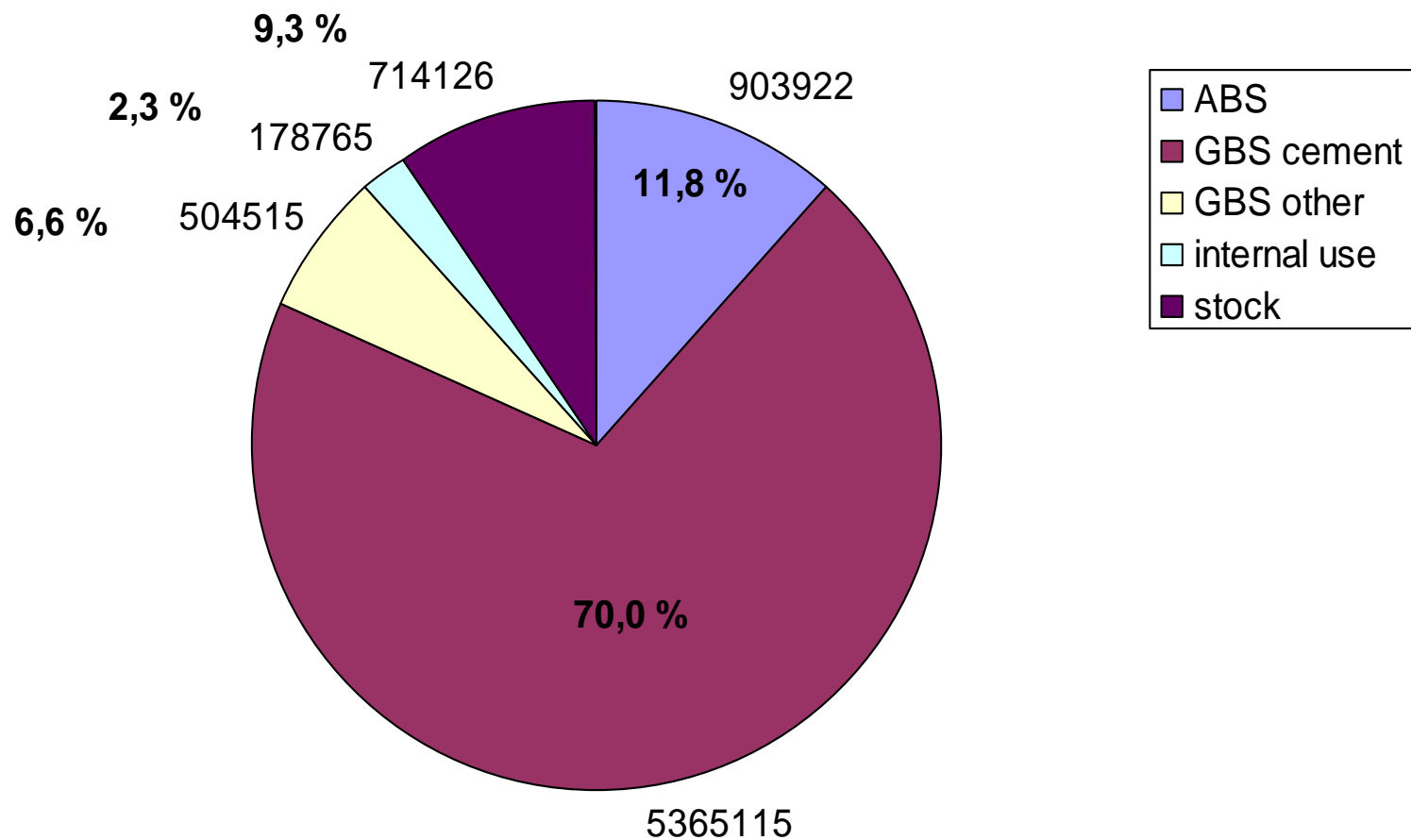


Use of Iron and Steel Slag in Europe 2008: 46.9 million tonnes



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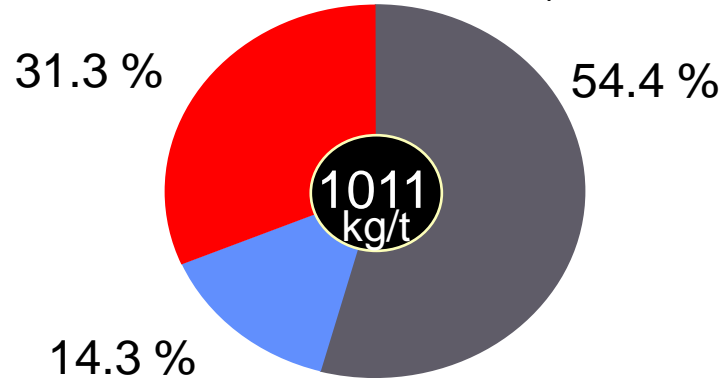
7,7 mio. t Blast Furnace Slags in Germany 2010



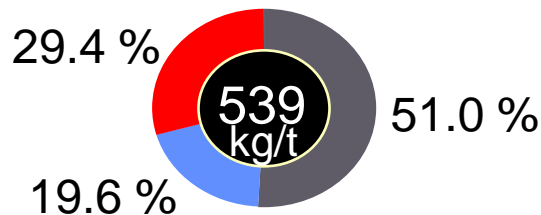
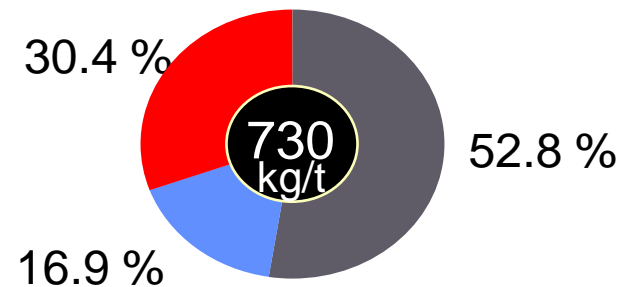
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Cement production and CO₂ emissions - Benefits of slag cements -

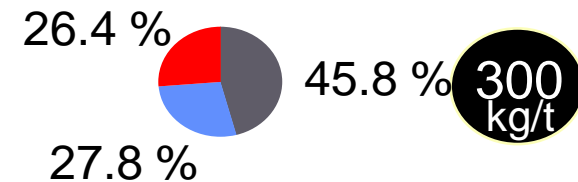
CEM I 32.5 R (= 100 %)



CEM II/B-S with 30 % slag (= 72 %)



CEM III/A with 50 % slag (= 53 %)

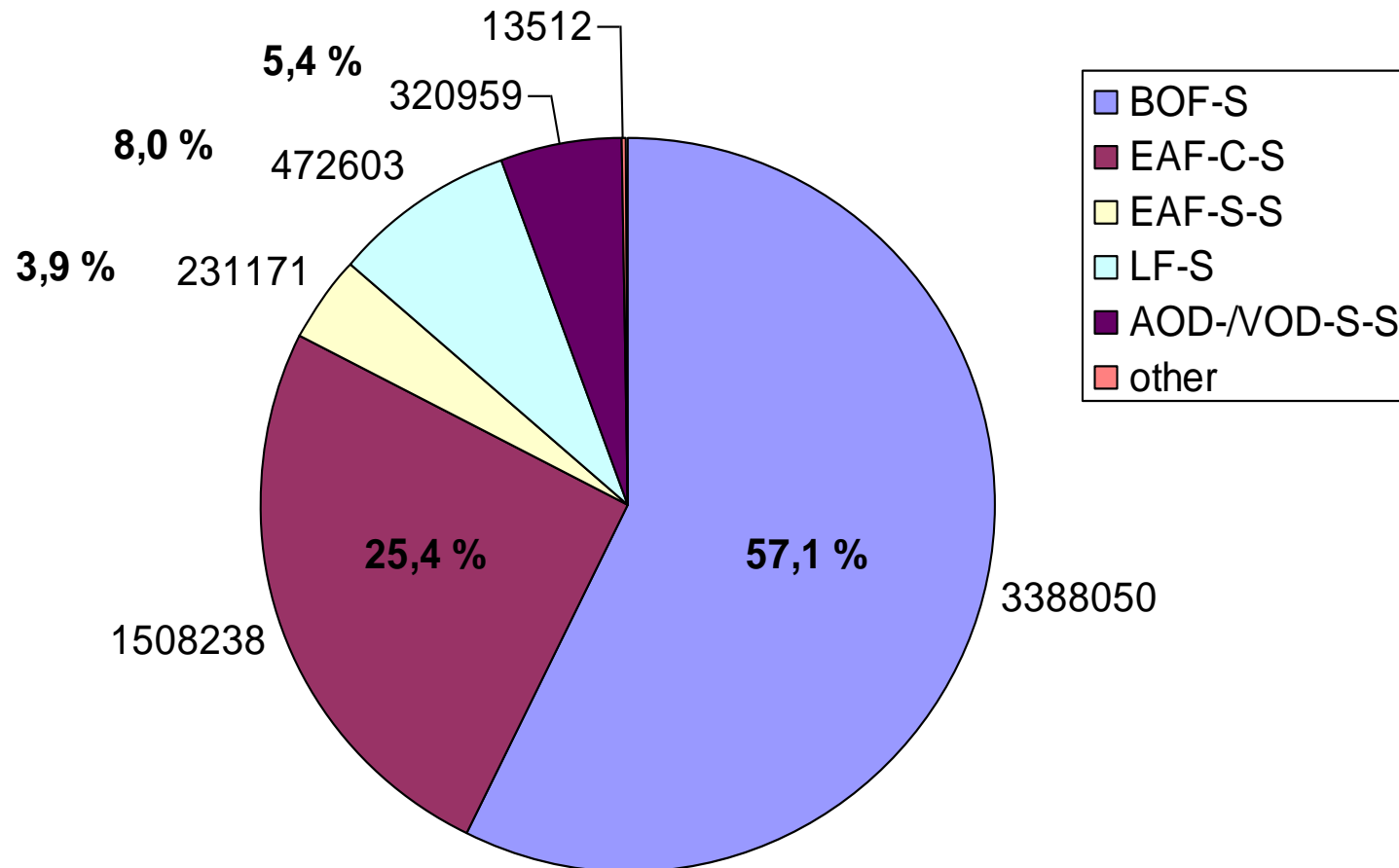


CEM III/B with 75 % slag (= 30 %)

Calcination: 0.55 t / t_{Cl}
 Electr. energy: 651 g/kWh
 Therm. energy: 331 g/kWh

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6 mio. t Steel Slags in Germany 2010

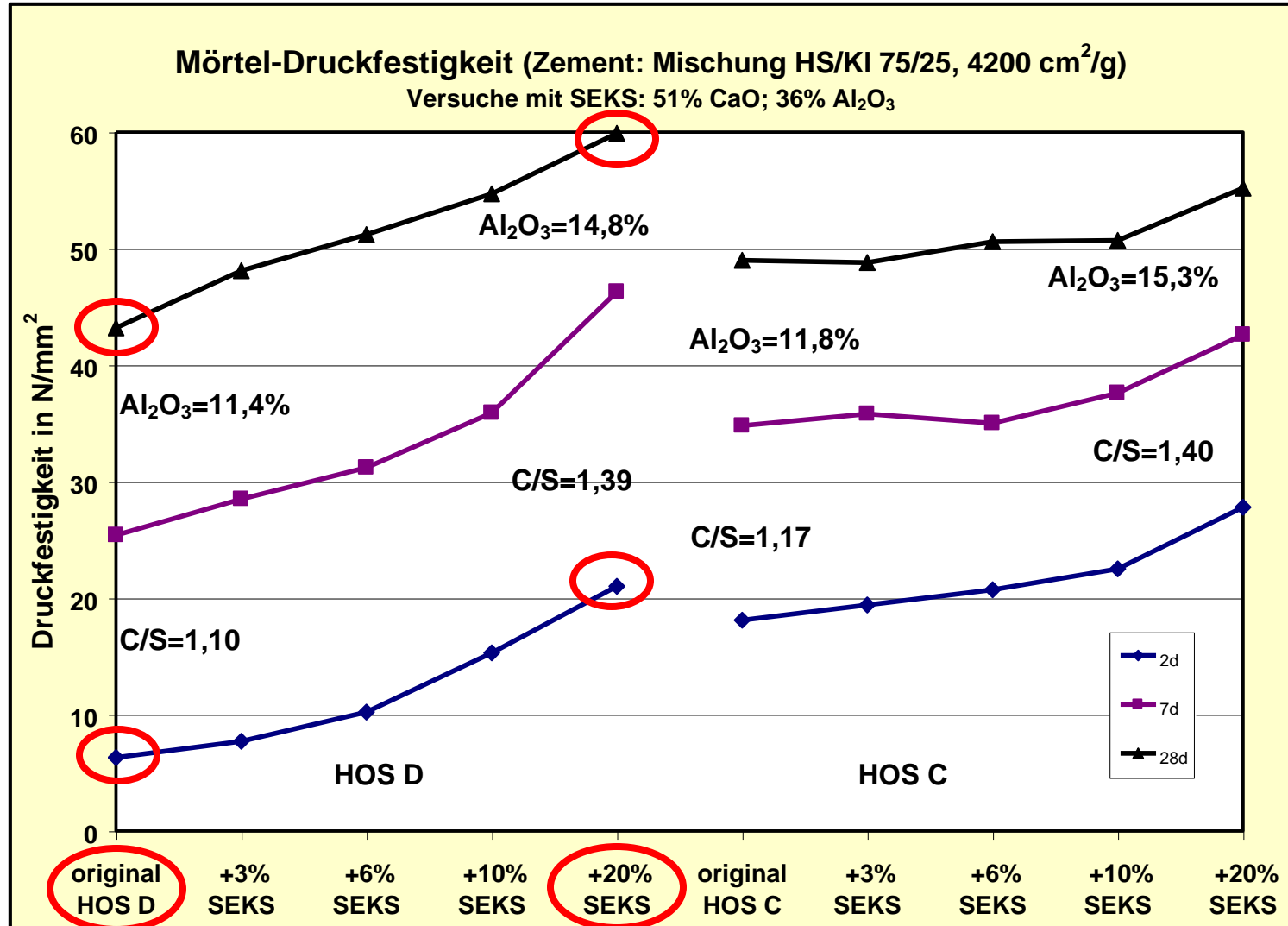


Increasing the quality of water granulated blast furnace slags

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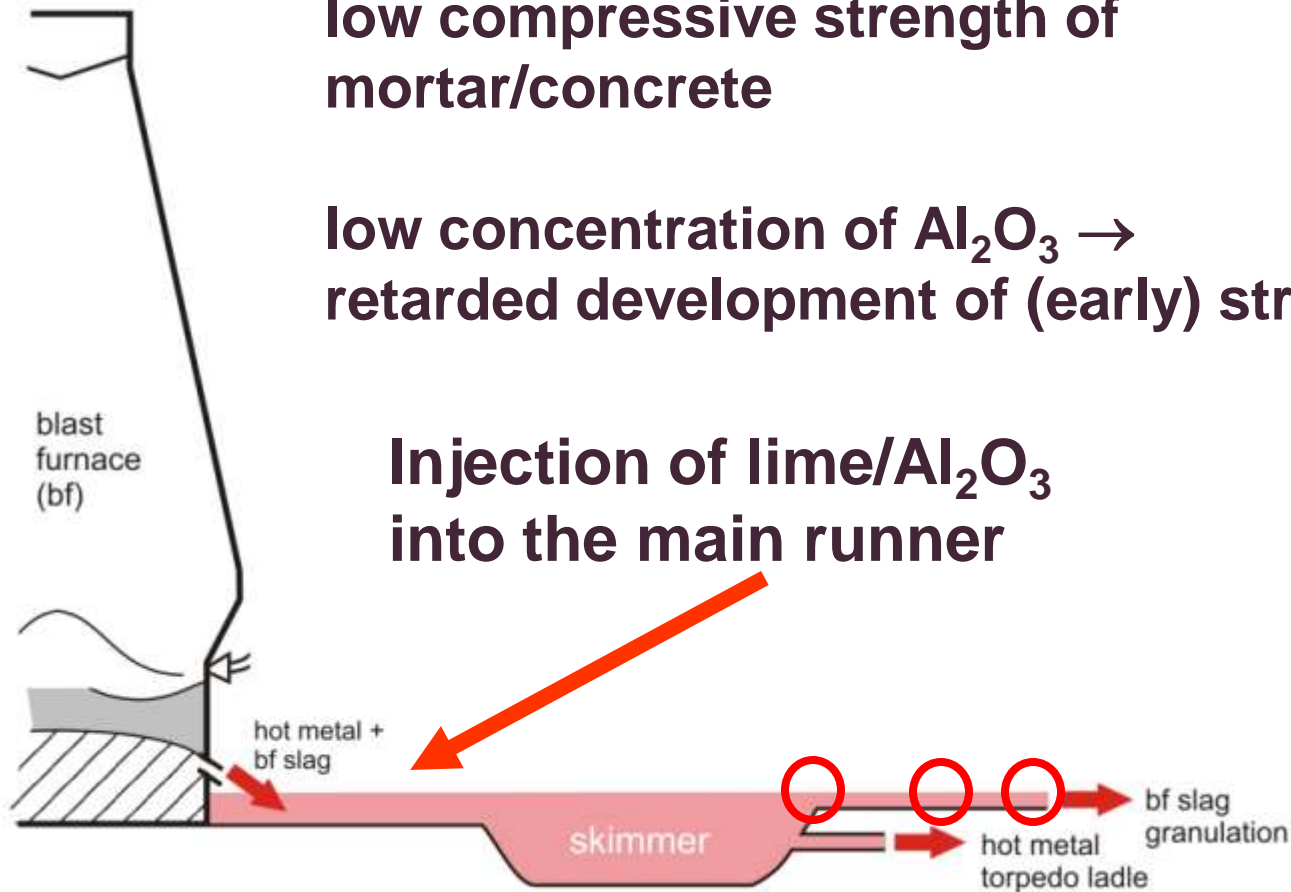


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**low basicity $\text{CaO}/\text{SiO}_2 \rightarrow$
low compressive strength of
mortar/concrete**

**low concentration of $\text{Al}_2\text{O}_3 \rightarrow$
retarded development of (early) strength**

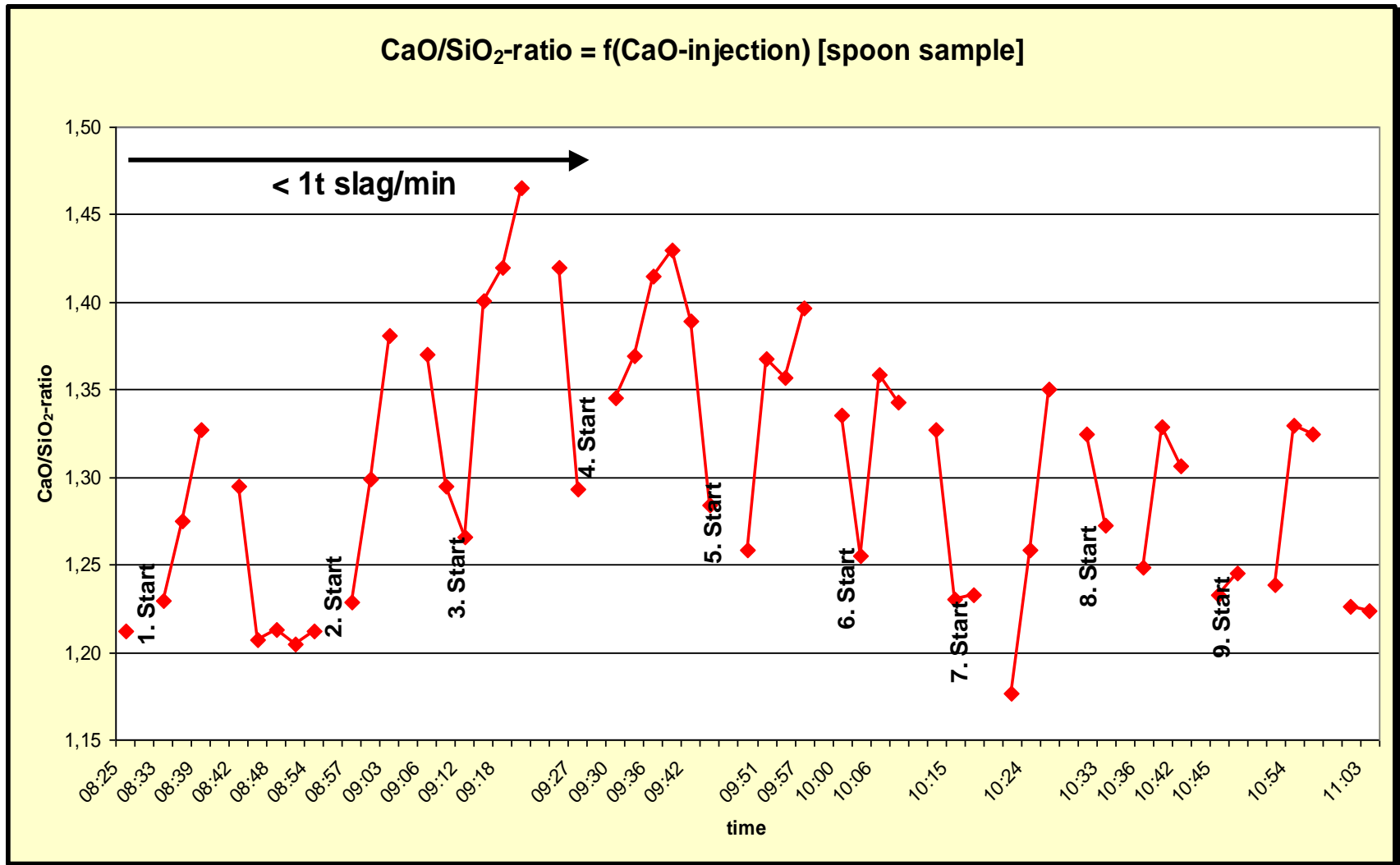
**Injection of lime/ Al_2O_3
into the main runner**



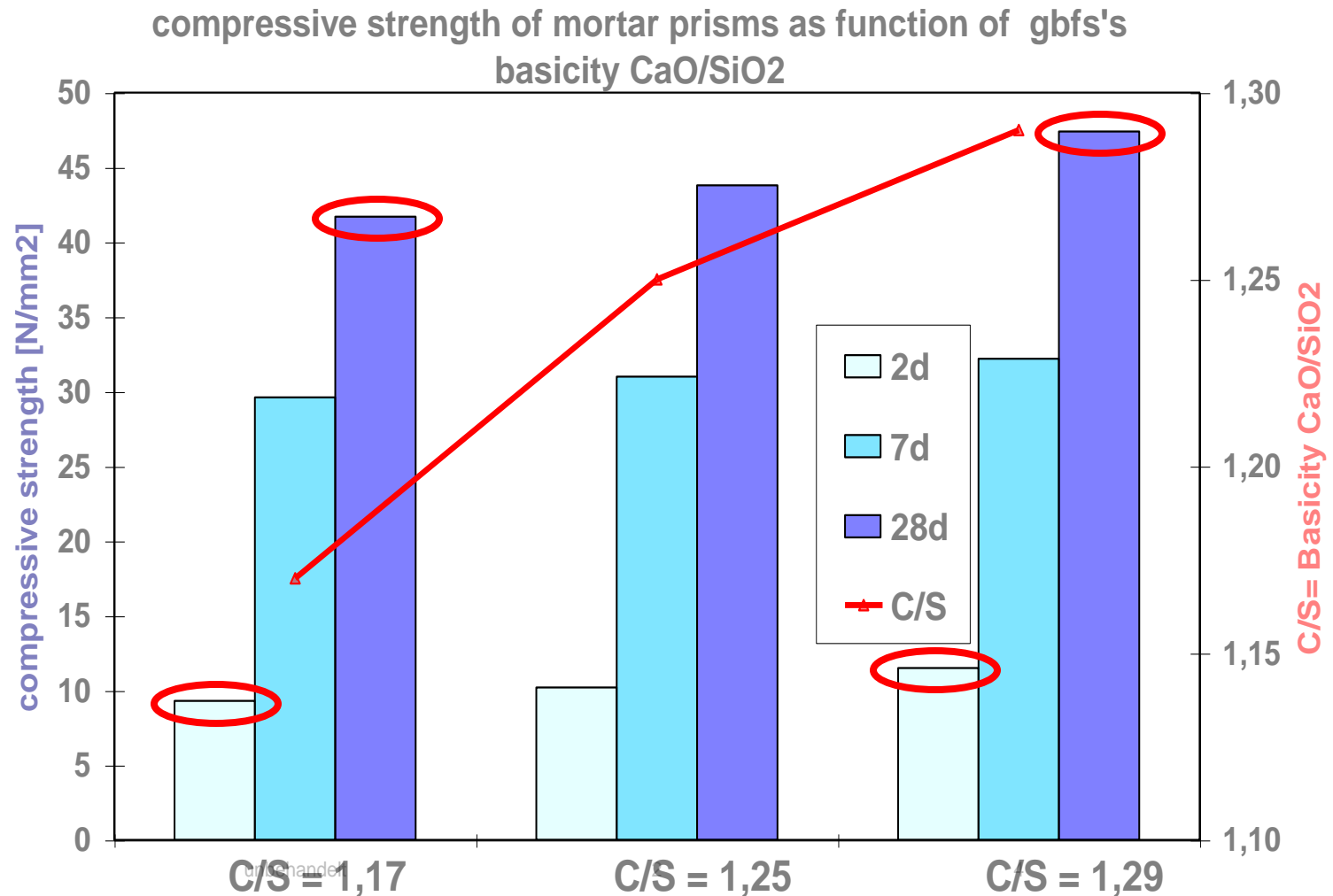
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Increasing the quality of basic oxygen furnace slags for the use in road construction

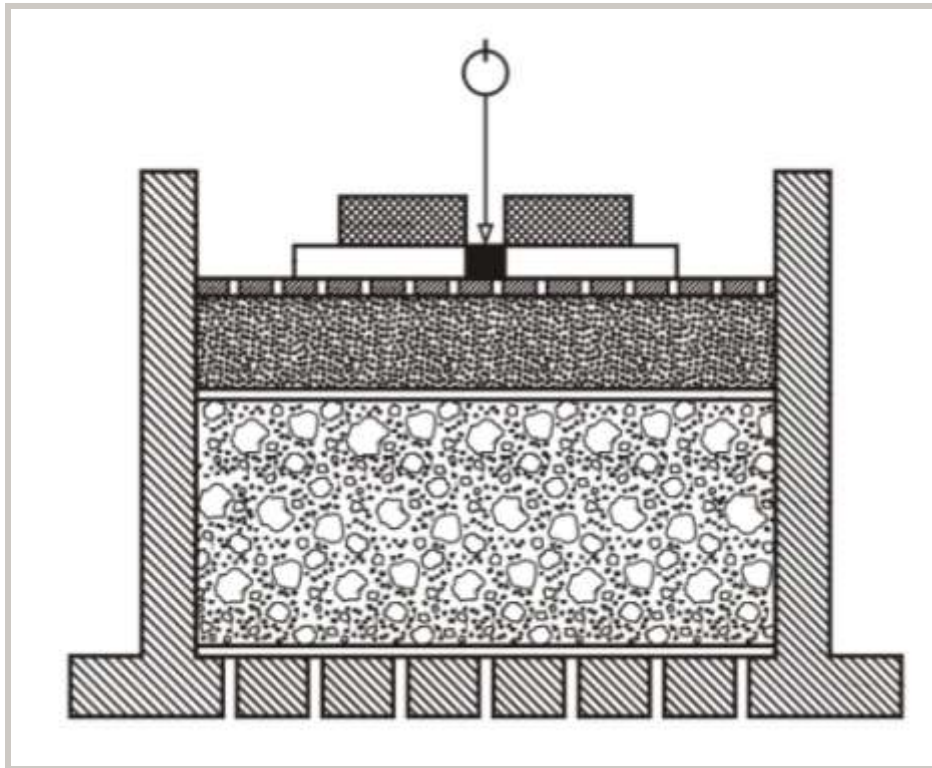
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BOF/EAF slag might have some free CaO (free lime) & free MgO (periclase). In the presence of humidity the hydration of both minerals causes 100 % increase in volume of the crystals.

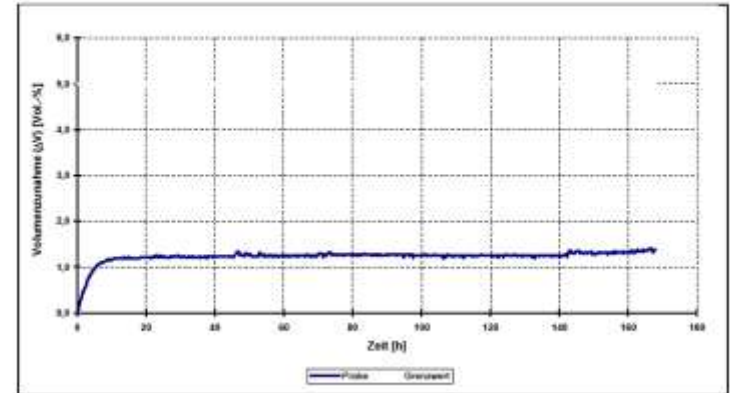


The hydration is a serious problem in using steel slag as construction material !

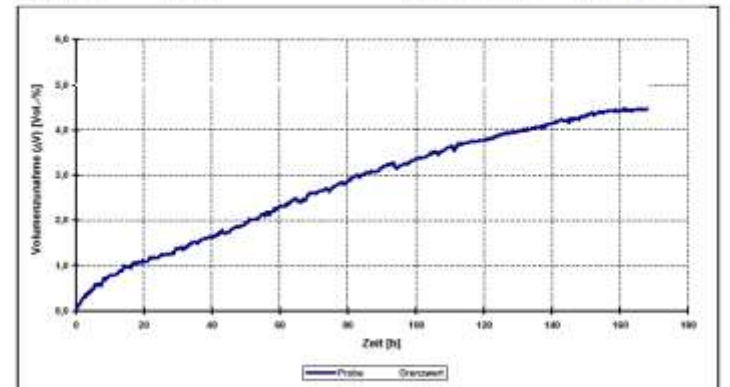
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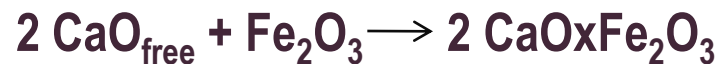
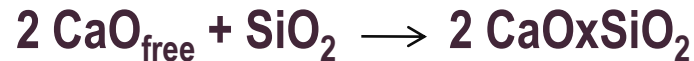
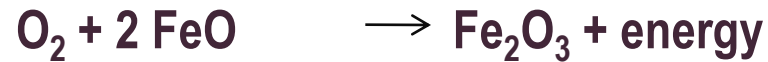
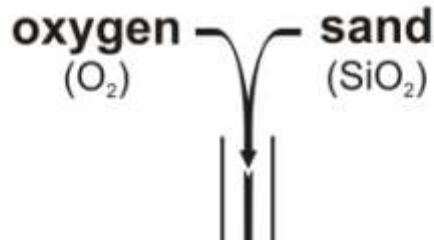
Raumbeständigkeit gemäß DIN EN 1744-1 (Dampfversuch)
 Auftraggeber / Herkunftsbauwerk: XXX XXX Datum: 19.12.2009
 Material: XXX XXX Volumenzunahme nach 24 h: 1,3 %
 Eingangsnummer: P2008-05205 Volumenzunahme nach 180 h: 1,4 %



Raumbeständigkeit gemäß DIN EN 1744-1 (Dampfversuch)
 Auftraggeber / Herkunftsbauwerk: FESG Datum: 15.08.2009
 Material: IS EGS f. Murnau Volumenzunahme nach 24 h: 1,2 %
 Eingangsnummer: P2008-05323 Volumenzunahme nach 192 h: 4,5 %

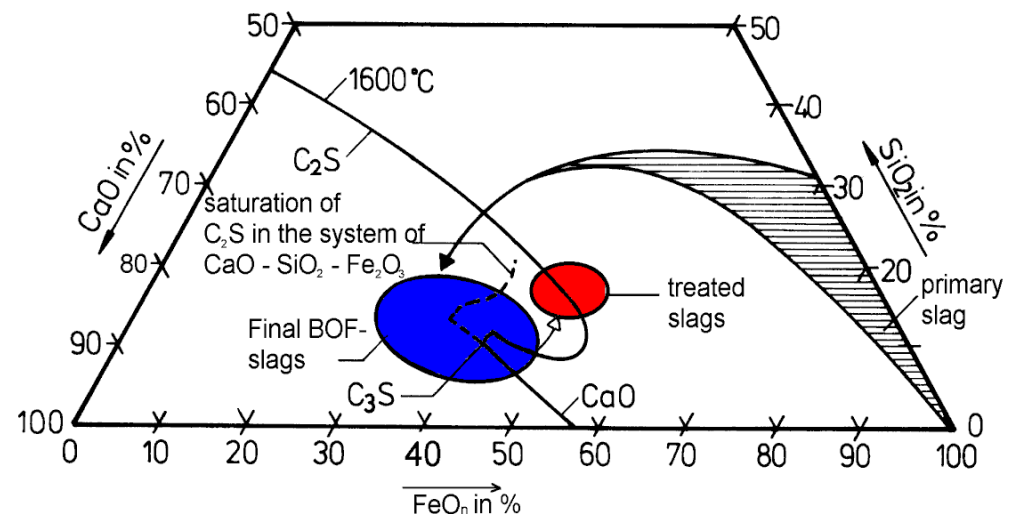


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by injection of sand and oxygen:

- ➔ additional heat is generated
- to keep slag liquid
- to heat up and dissolve the sand

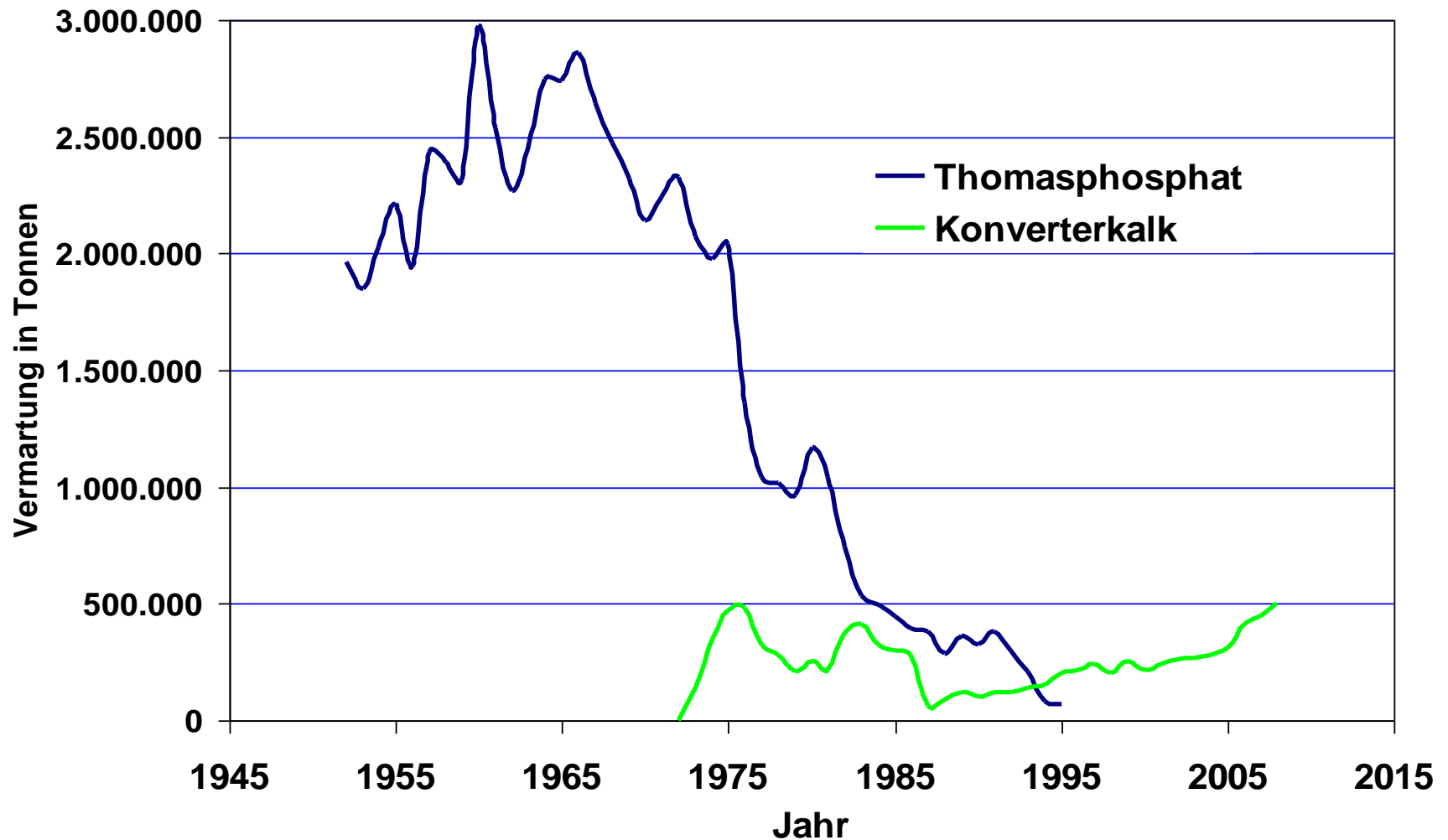


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Increasing the quality of basic oxygen furnace slags for the use as fertiliser

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Aim:

sewage sludge ash + BOFS → „Thomasphosphate 2nd Generation“
~ 20 % P₂O₅ ~ 1,5 % P₂O₅ ~ 10 % P₂O₅
with ~ 40 % ~ 95 % ~ 99 % available for plants

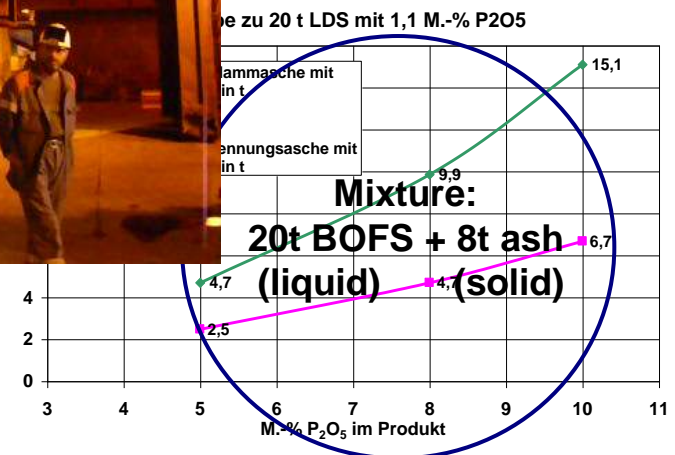
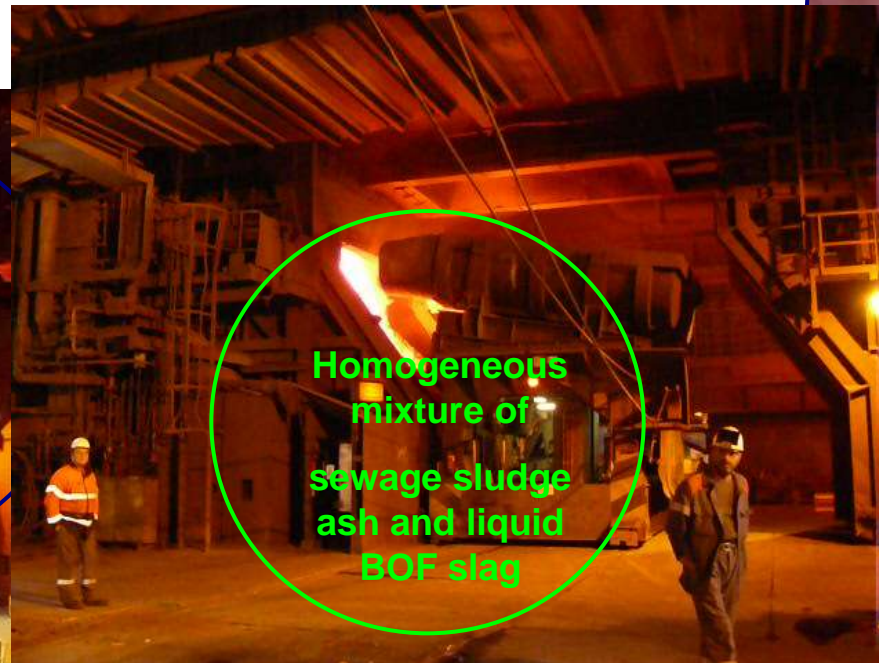
Whitlockite + Dicalciumsilicate → Calcium-Phosphate-Silicate



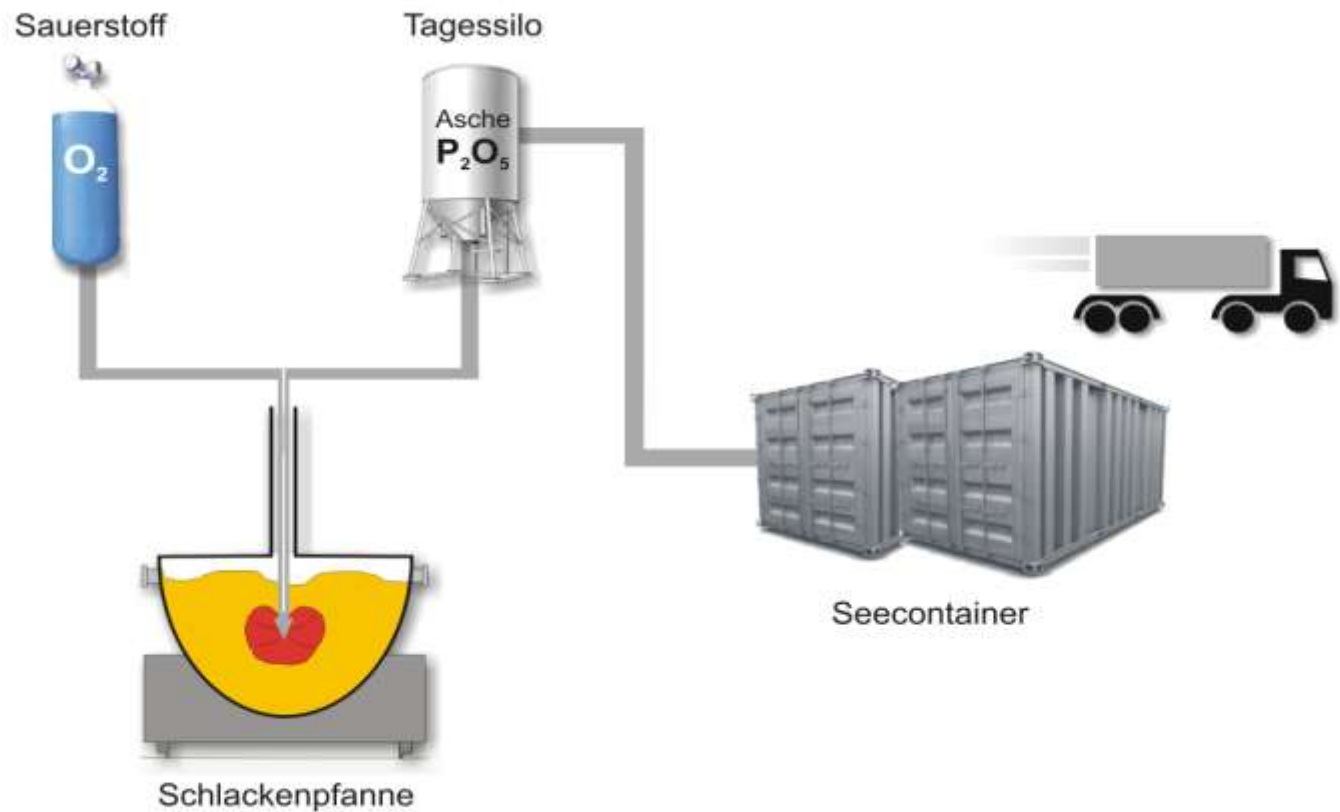
Approach:

dissolution of the ash in the liquid slag

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Optimising the metallurgical work of electric furnace slags

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leitet nach Sendung	52 - 40	3 - 1	3 - 2	2 - 12	0'2 - 3	2 - 30	0'1 - 0'5
Stahler-	Fe_2O_3	SiO_2	CaO	Al_2O_3	MnO	MgO	P_2O_5
leitet nicht	52 - 42	3 - 1	3 - 2	1 - 2	0'1 - 1	12 - 32	0'1 - 1'2



Steel

EAF-Slag

Recycling/Utilisation:

Scandust/Valera

Internal Recycling

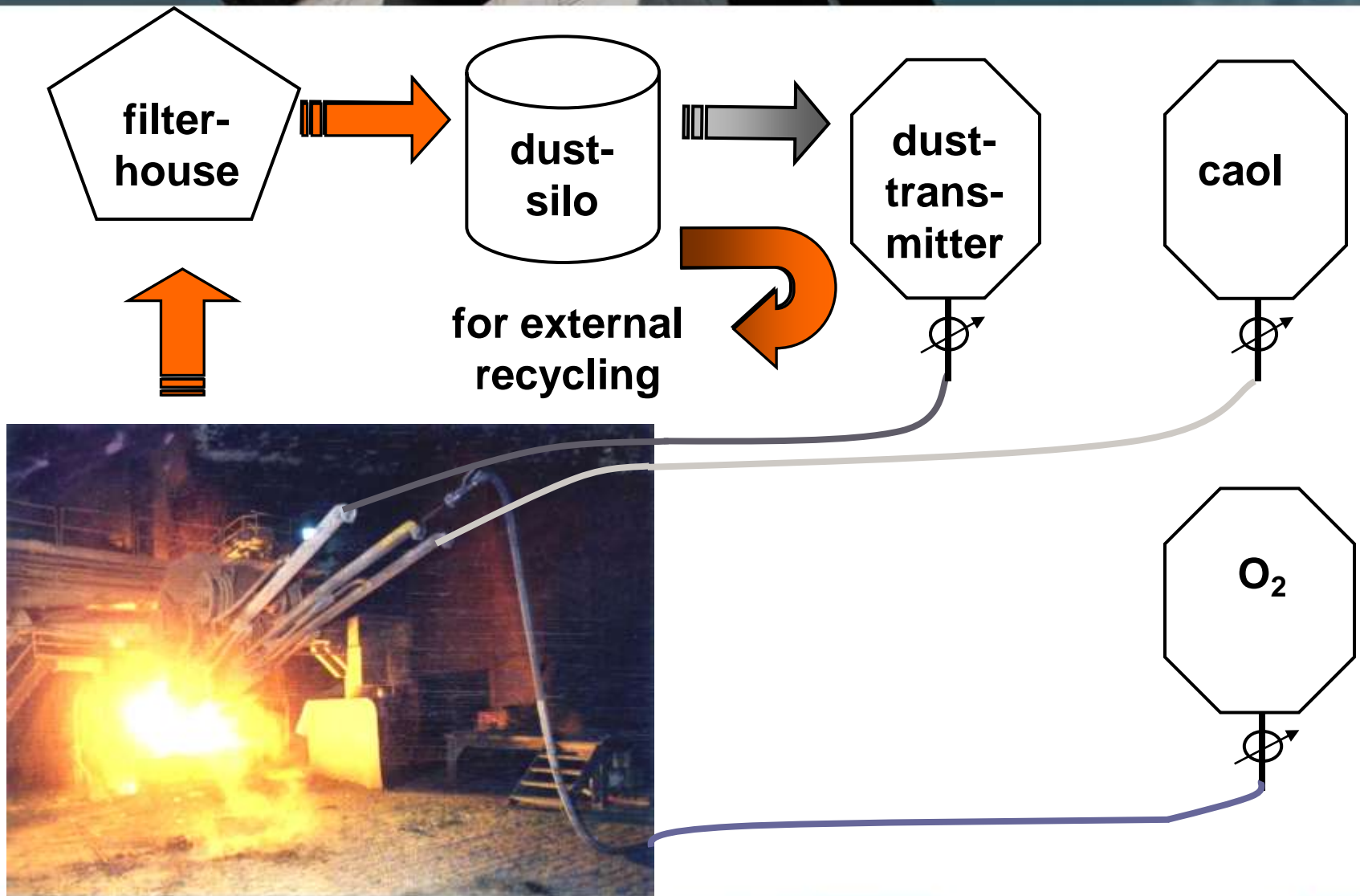
Stope filling

Waelz kiln

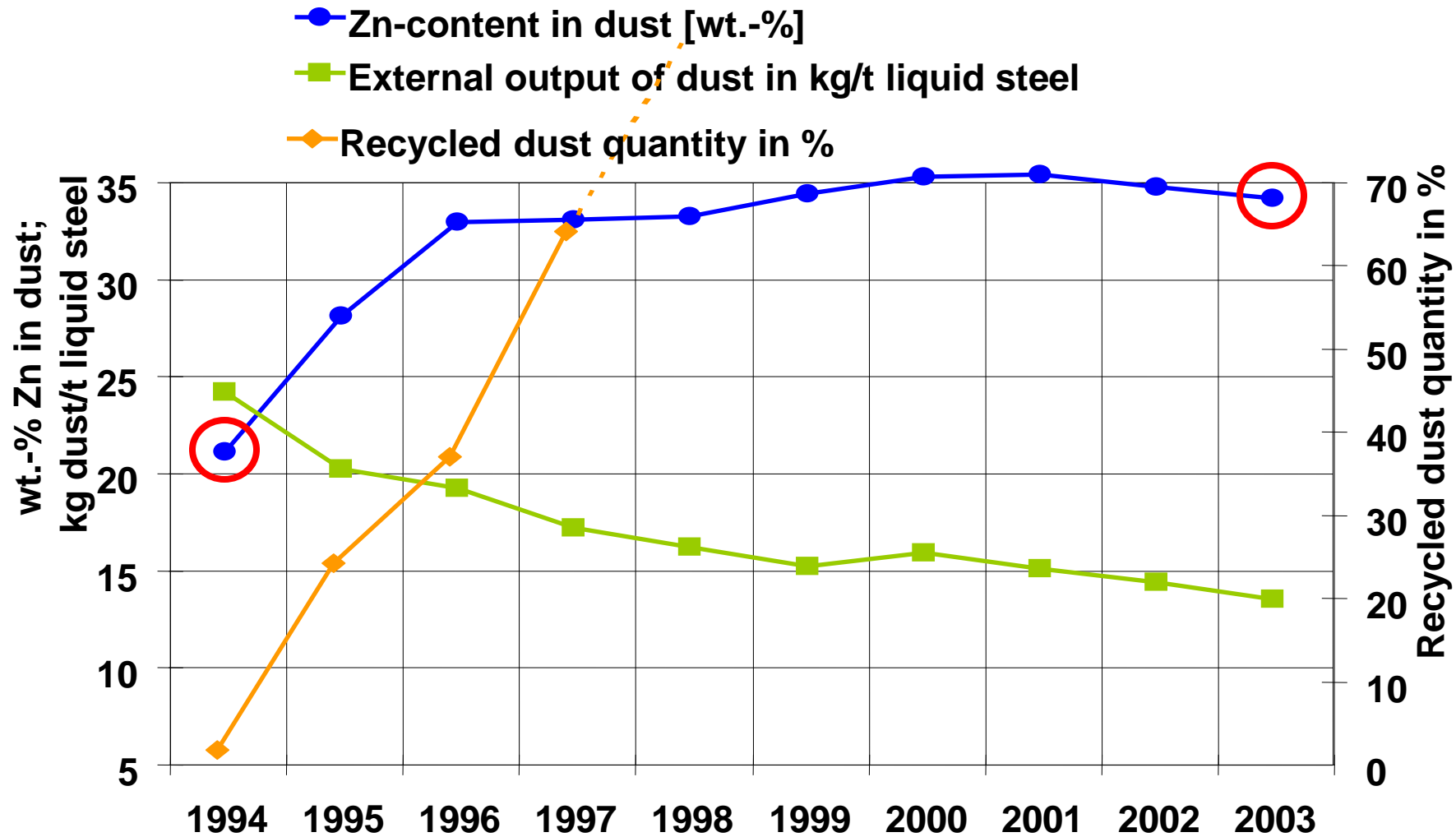
Waelz
Oxide

Waelz
Slag

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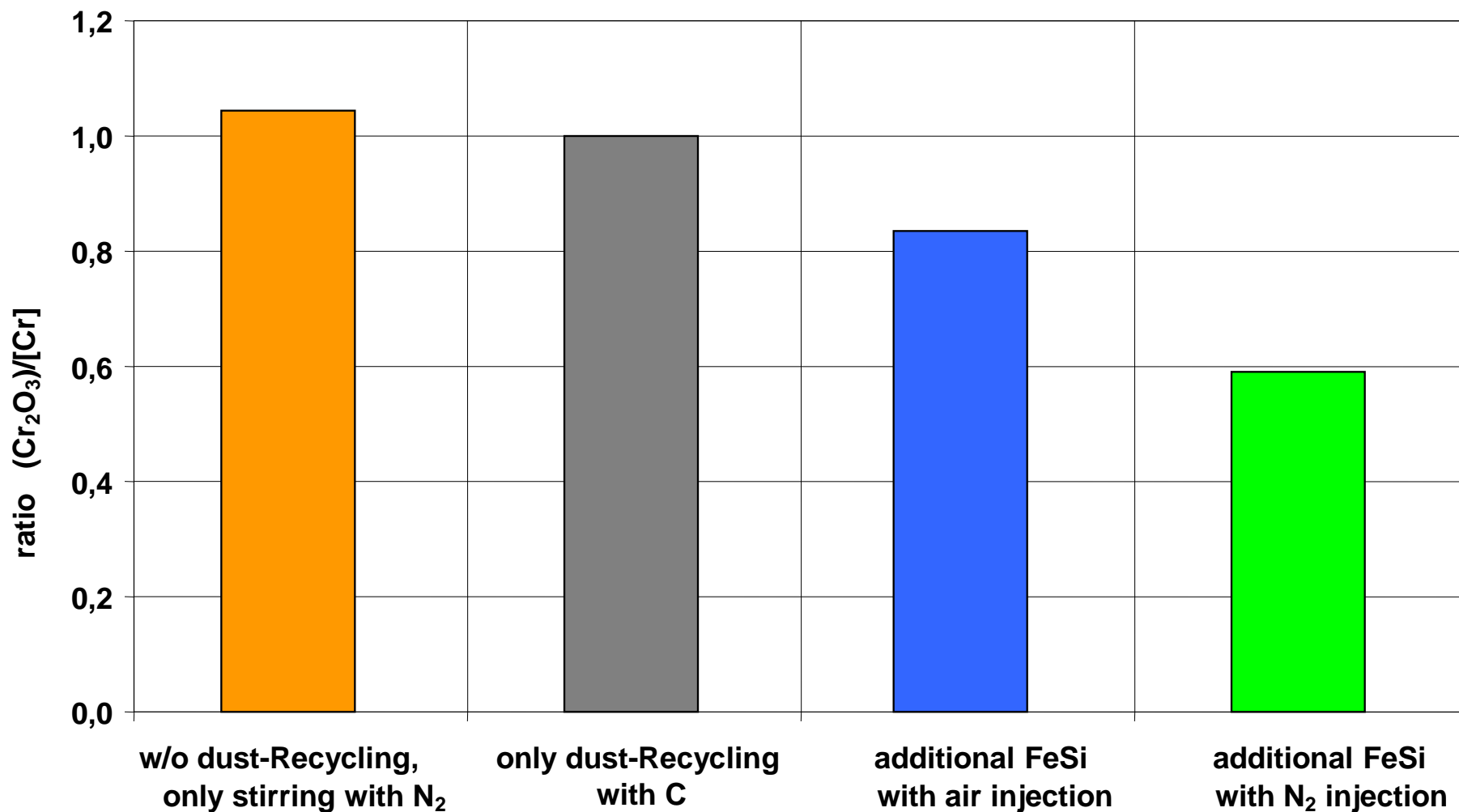


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Chrome scorification as function of treatment



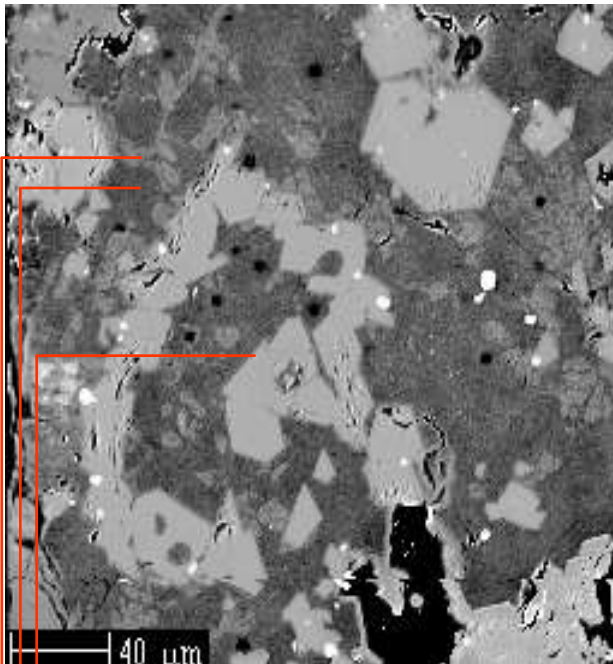
Increasing the quality of stainless steel slags

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Compared to 19 wt.-% Cr_2O_3 in solid material, the leaching of 0.7 mg Cr/liter slag is surprisingly low.

95 % of the total Cr is fixed as chromite, a Spinel-type mineral.

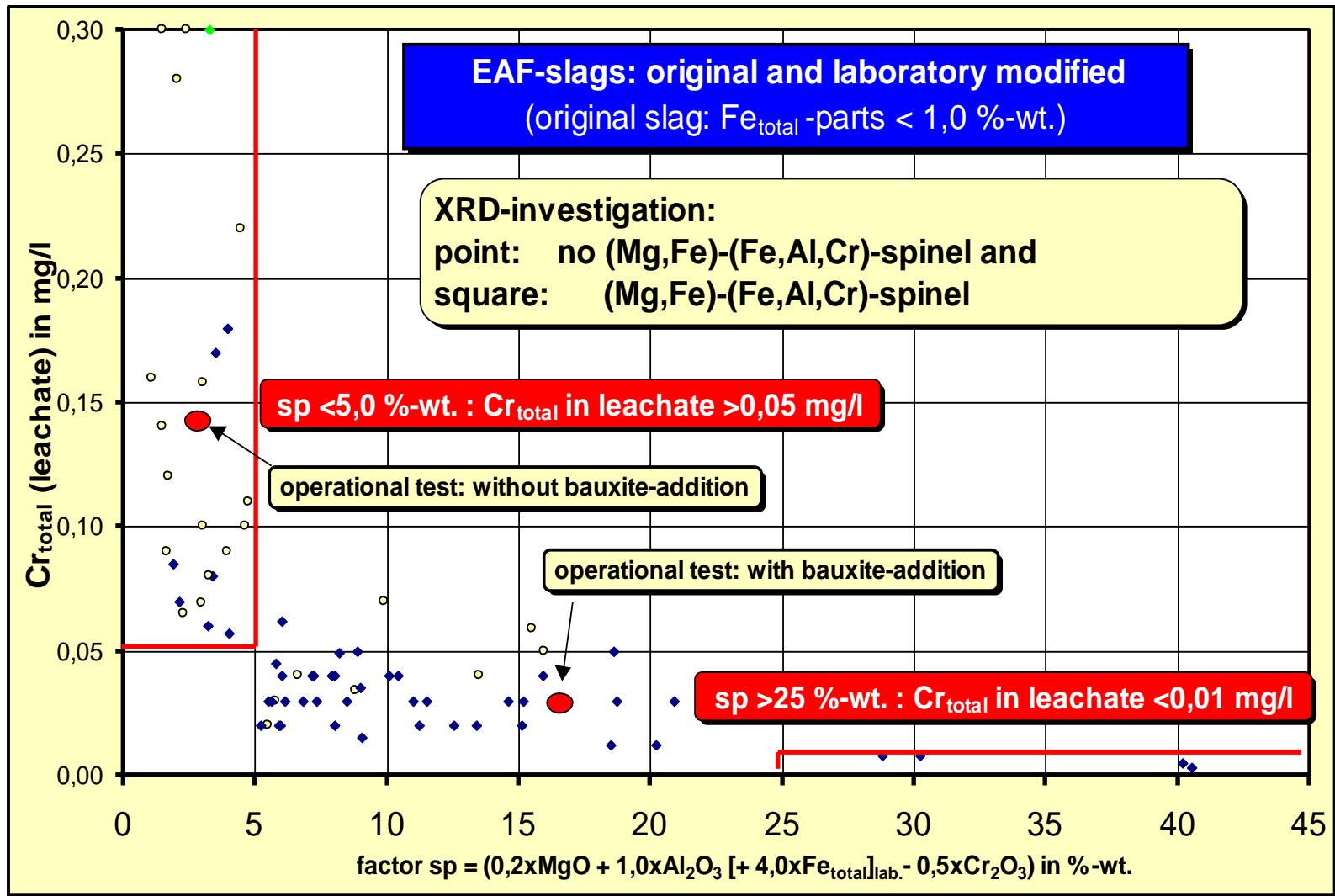
($\text{Me}^{2+}\text{Me}_2^{3+}\text{O}_4$, with $\text{Me}^{2+} = \text{Fe}^{2+}, \text{Mg}^{2+}, \text{Ni}^{2+}$ and $\text{Me}^{3+} = \text{Fe}^{3+}, \text{Al}^{3+}, \text{Cr}^{3+}$) are known to be very stable under environmental conditions. Further progress is possible by stimulating the formation of spinels.



Mineral:	Idealised Formula:	% of Mineral:	Electron Microprobe Analyses of Minerals [wt.-%]										
			SiO_2	Al_2O_3	CaO	MgO	Cr_2O_3	MnO	Fe_2O_3	NiO	MoO ₃	P ₂ O ₅	S
Merrillite	$\text{Ca}_2\text{Al}_2\text{SiO}_7$	20	33,3	14,1	37,9	2,2	0,1	10,9	0,1	0,03	0,00	0,10	0,53
Bredigite	$\text{Ca}_7\text{MgSi}_4\text{O}_8$	45	34,3	0,1	46,5	10,4	1,4	2,4	2,5	0,01	0,01	0,08	0,02

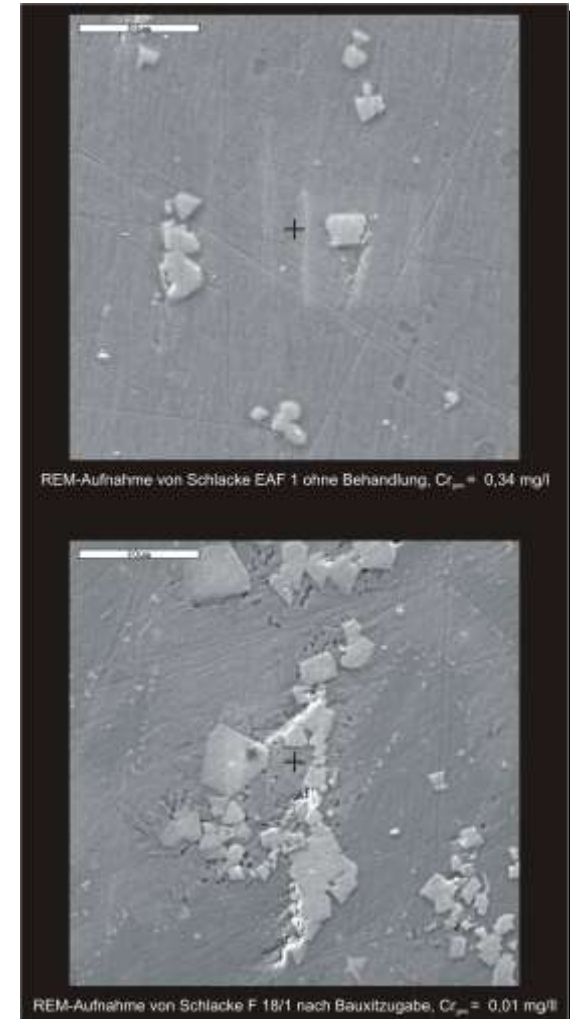
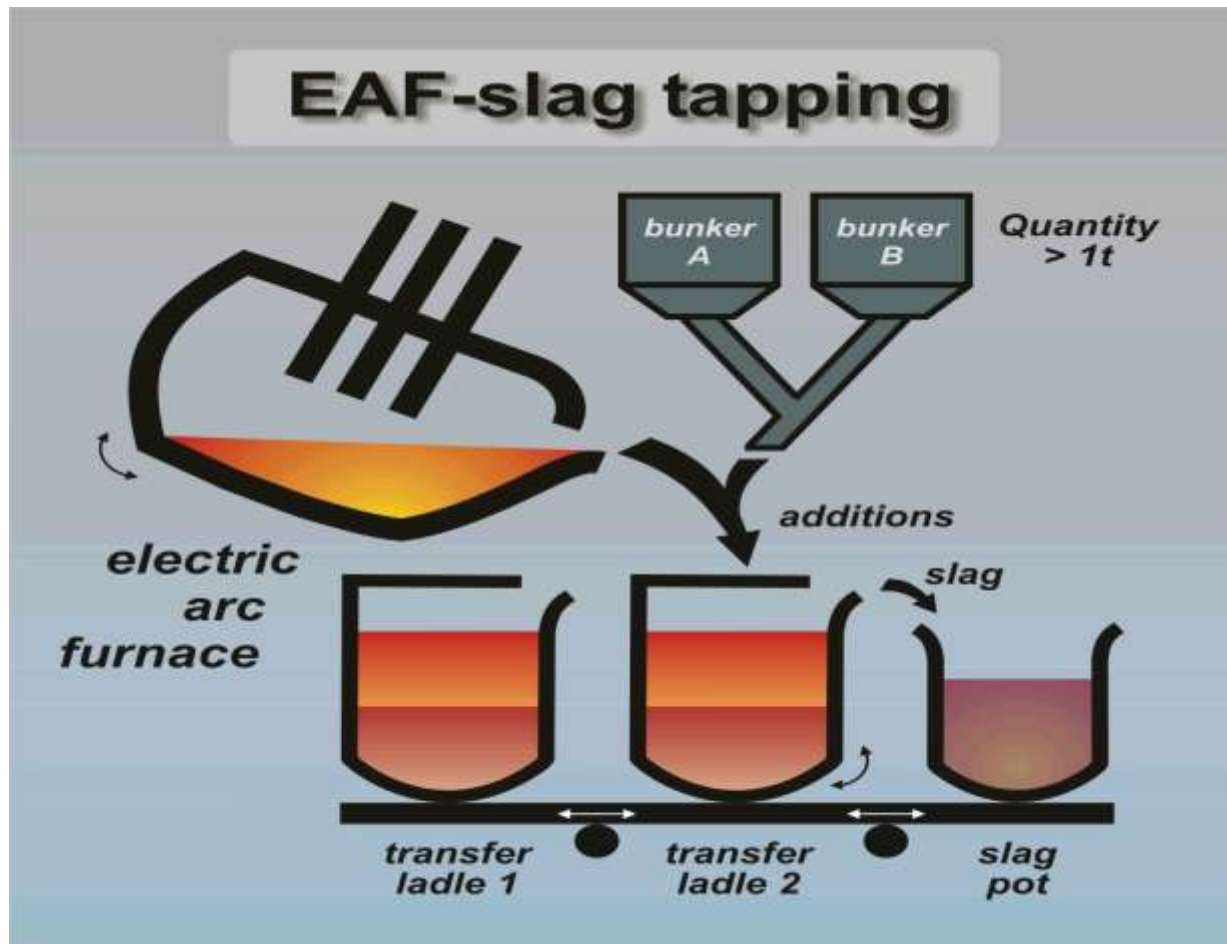
$$\text{Factor SP} = 0.2 \text{ MgO} + 1.0 \text{ Al}_2\text{O}_3 + n \text{ Fe}_{\text{total}} + 0.5 \text{ Cr}_2\text{O}_3$$

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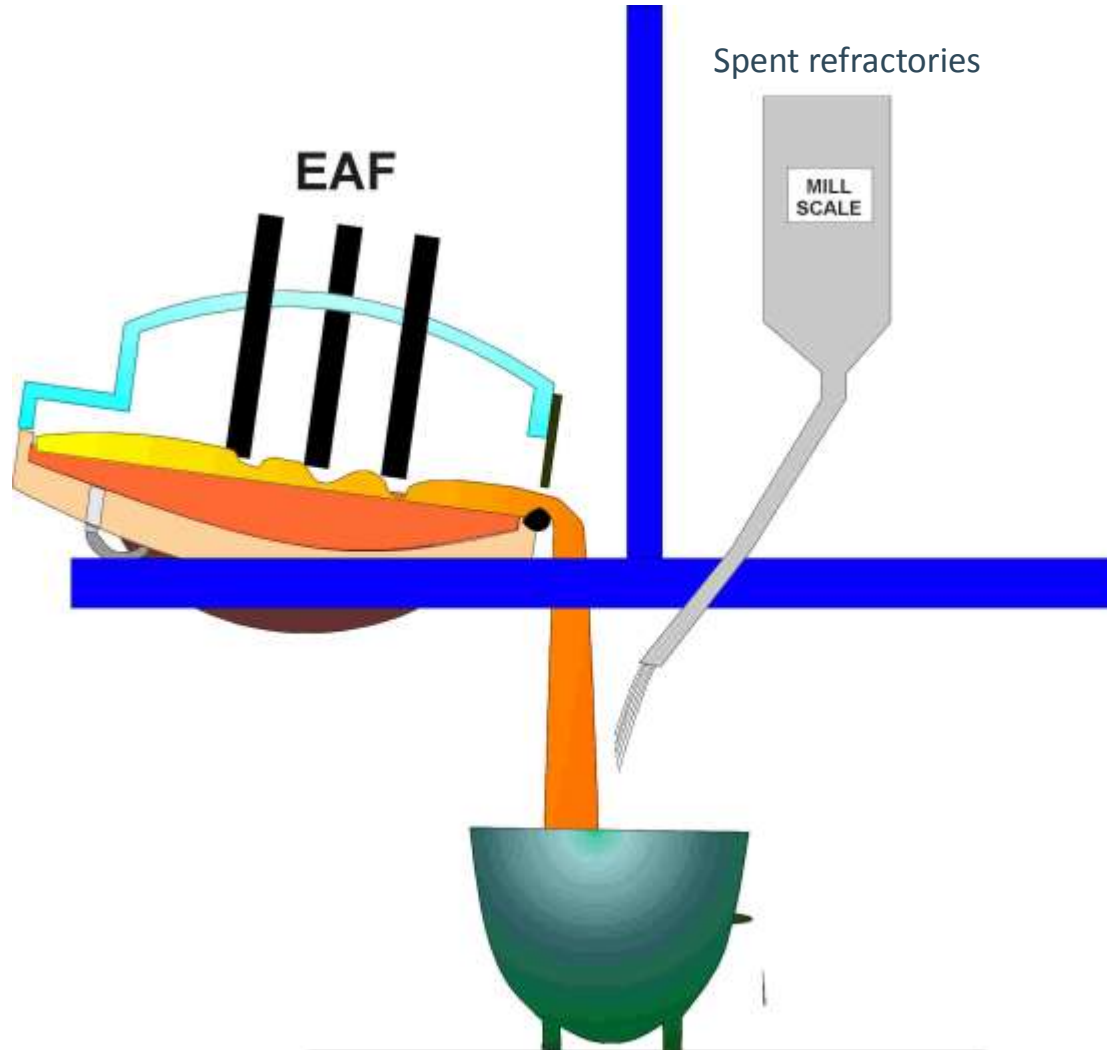


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Operational tests



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Increasing the quality and optimising the recycling of secondary metallurgy slags

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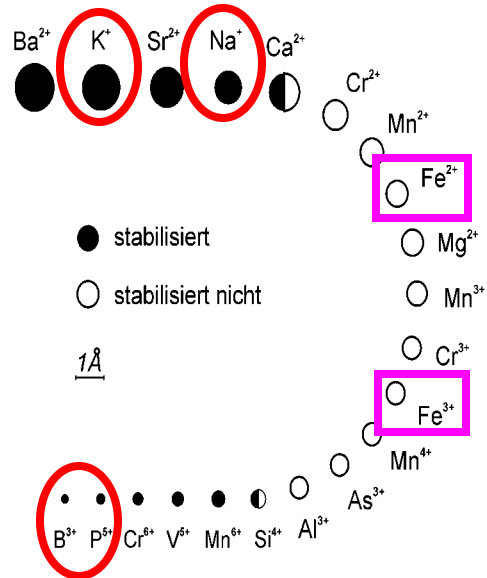
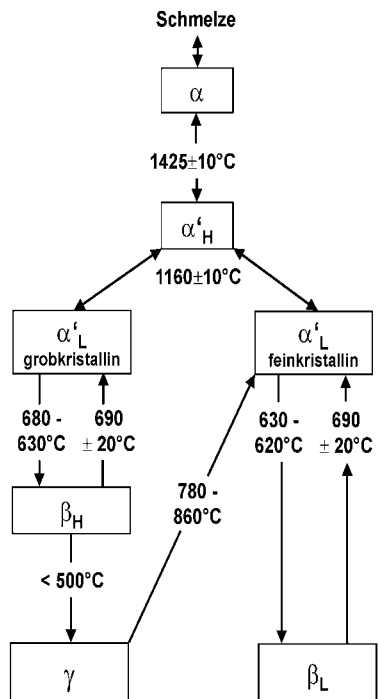
During solidification of secondary steelmaking slag some dicalciumsilicate (C_2S) is built, mostly. By further cooling C_2S transforms from β - to γ - modification. The transformation is accompanied by an increase in volume of 11 % of the crystals. The increase in volume destroys the structure of slag.

The transformation causes several problems:

- ⊗ formation of dust,
- ⊗ fine grained materials are hardly used in civil engineering,
- ⊗ progressive leaching according to the high specific surface area.

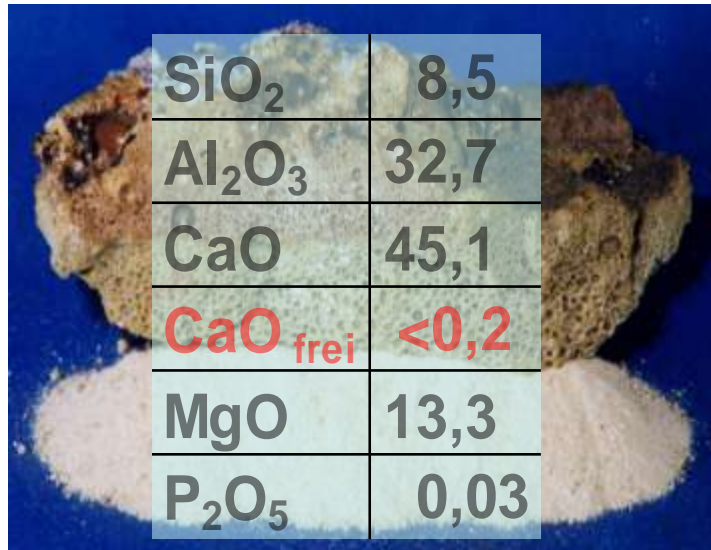
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Phasenumwandlungen des Dicalciumsilikats - C₂S -



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■ Solution 1 : rapid cooling of the slag



SiO ₂	8,5
Al ₂ O ₃	32,7
CaO	45,1
CaO _{frei}	<0,2
MgO	13,3
P ₂ O ₅	0,03

cooling-rate (K/min)	amorphous	Periclase (MgO)	beta-C2S (Ca ₂ SiO ₄)	gamma-C2S (Ca ₂ SiO ₄)	Mayenite (Ca ₁₂ Al ₁₄ O ₃₃)
> 1 - 5	X	X	X		X
porous	*	X	X		X
< 1		X	X	X	X

■ Solution 2: Addition of stabilising elements to the liquid slag

The transformation of C₂S is suppressed by distinct elements like P and B. For example in BOF slag the transformation is suppressed by the already available P₂O₅ (1.3 - 2.1 %). B is more efficient as ≈ 0.5 % B ensures stabilisation of LF-slag.



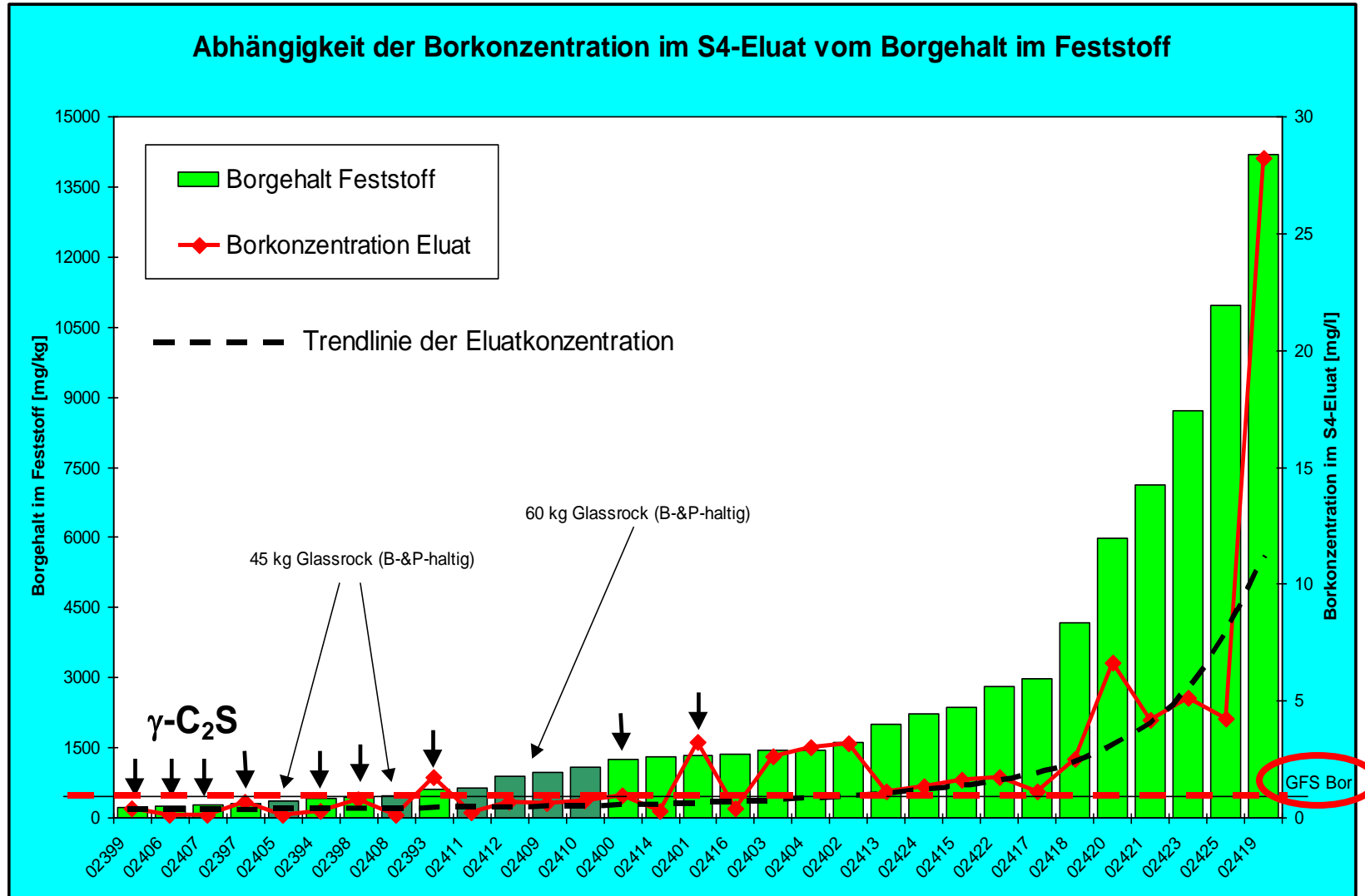
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Conclusion

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